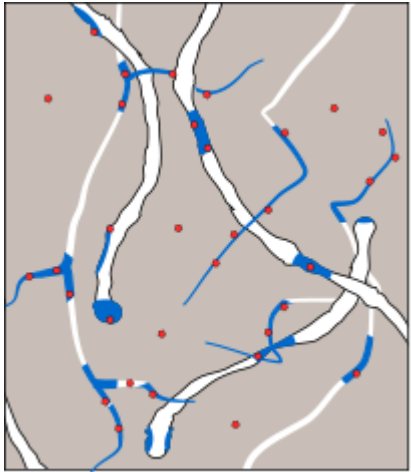


DOES MACROPORE FLOW IN NO-TILL SYSTEMS FLUSH OR BYPASS MOBILE SOIL NITROGEN AFTER HARVEST?

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Background

Mobile N after harvest



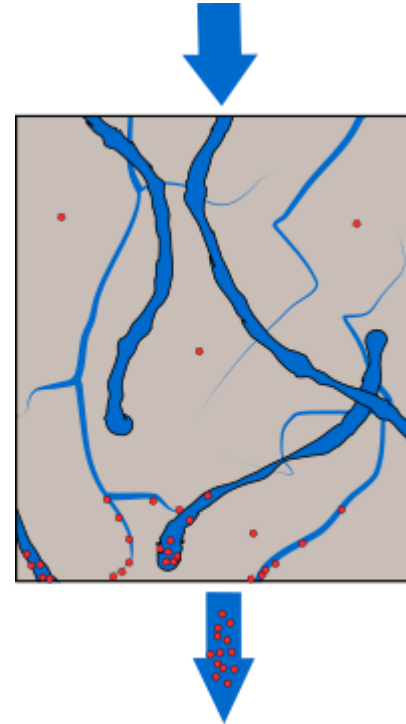
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Macropore flow

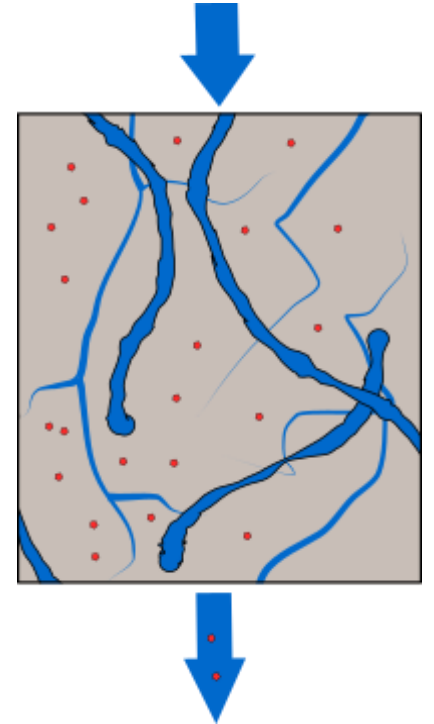


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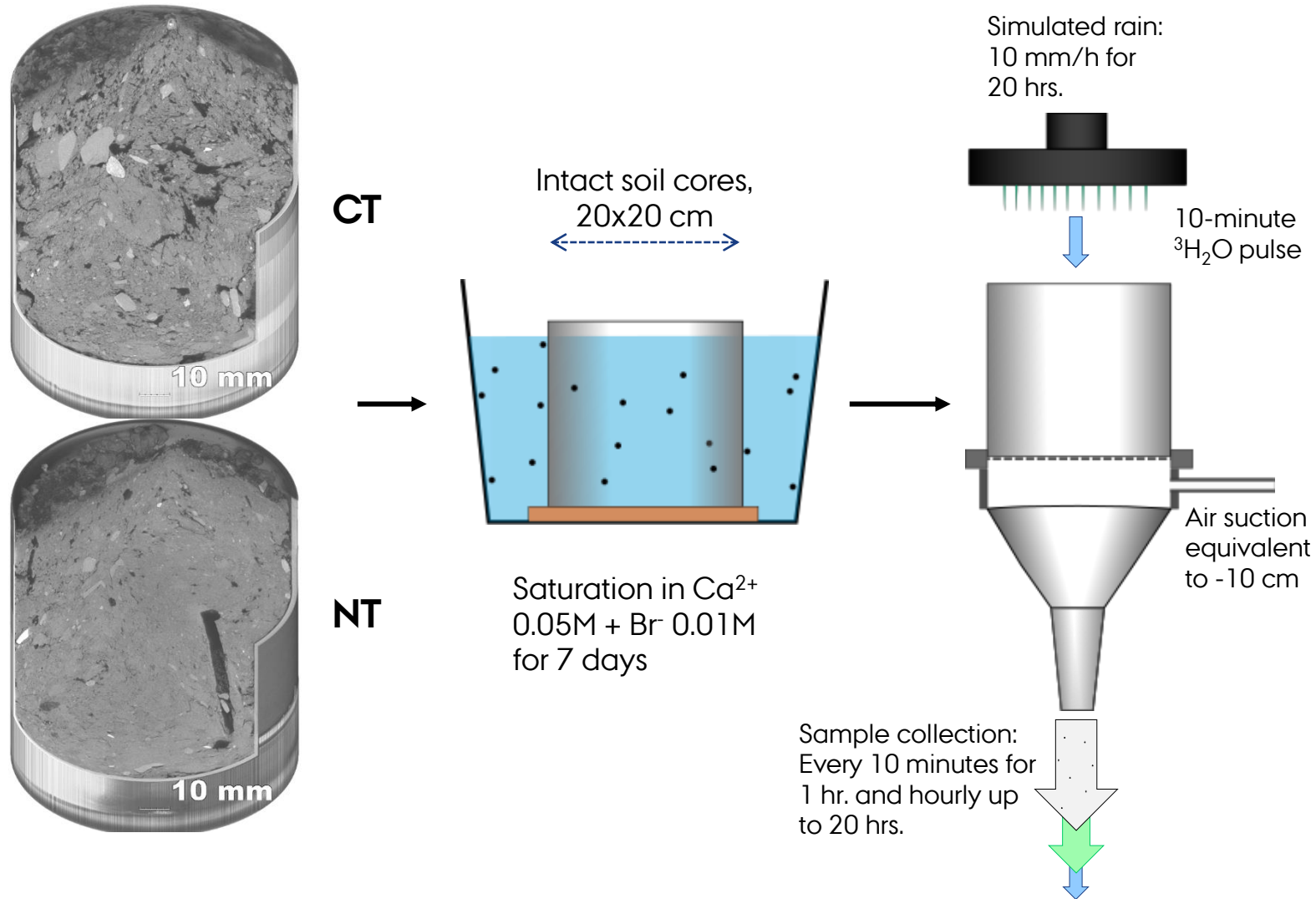
Increased or reduced leaching?



OR



The study in very few words:



2 Tillage treatments:

- Conventional Till (CT)
- No-till (NT)

2 Sets of intact cores

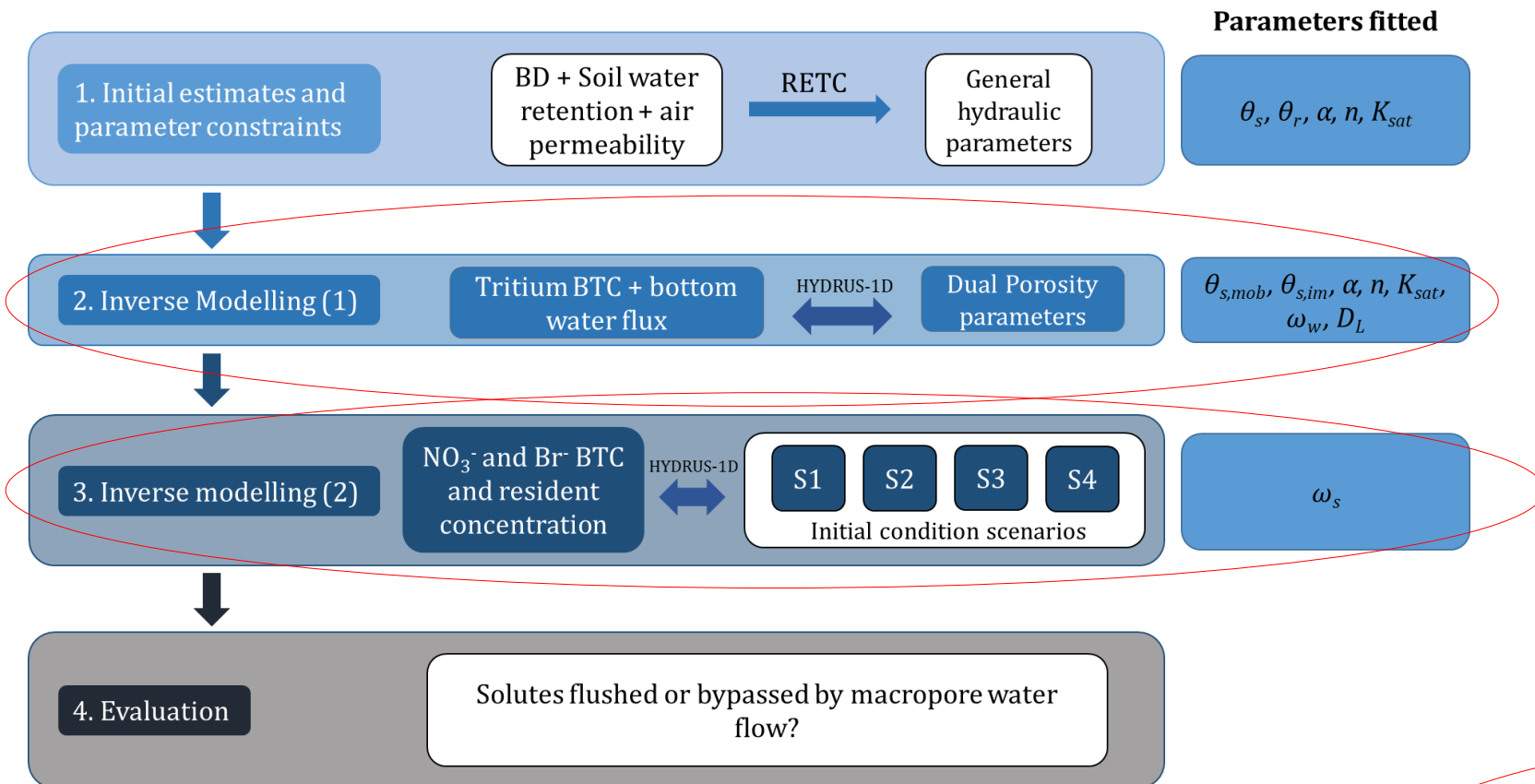
- Reference (only soaking)
- Experimental (soaking + simulated rain)

3 tracers:

- Tritium pulse
- Bromide added by soaking
- Native NO_3^- (from the field)

2 main analyses:

- BTCs (^3H , Br , NO_3^-)
- Dissection at 4 depths



Modelling work distributed over several rounds of inverse modelling

Inverse modelling in HYDRUS-1D:

- Dual porosity (mobile-immobile) water flow
- Dual porosity (mobile-immobile) solute transport
- Van Genuchten-Mualem theory
- Richard's equation and advection dispersion functions in the mobile phase
- No vertical flow or solute movement in immobile phase
- 1st-order kinetics mass transfer of water and solutes between phases (horizontal movement)

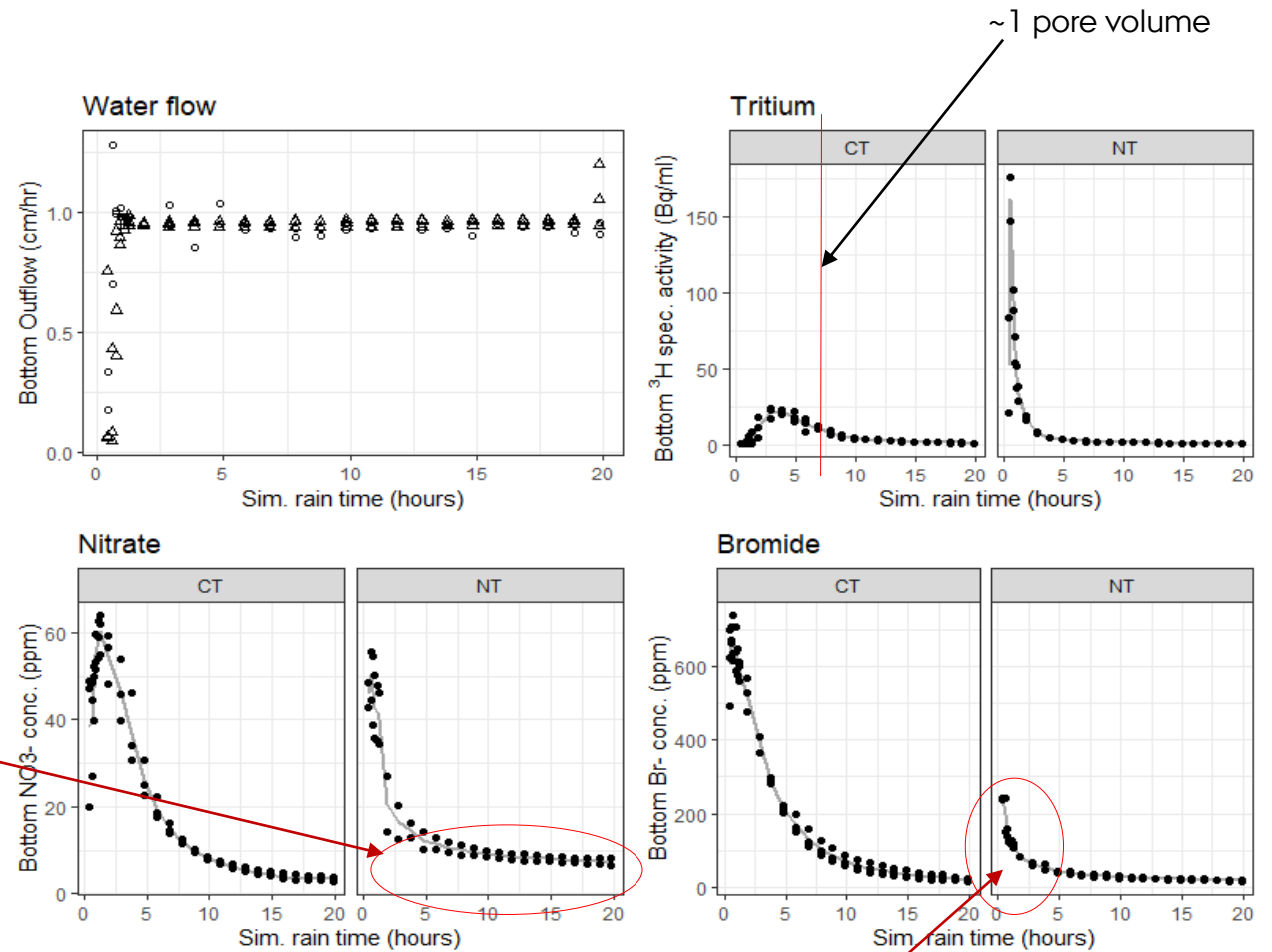
Four initial solute distribution scenarios:

S1	S2	S3	S4
$C_{mob} = C_{im}$	$C_{im} = 0$	$C_{mob} = 0$	Manually adjusted



Breakthrough curves

- Rapid initiation of drainage
- Quick pulse leaching of Tritium in NT
- Some degree of macropore flow in CT
- Earlier leaching of bromide and nitrate
- “Tail” of leached nitrate in NT only
- Limited infiltration of bromide in NT



Nitrate “tail”

Minimal Br intrusion

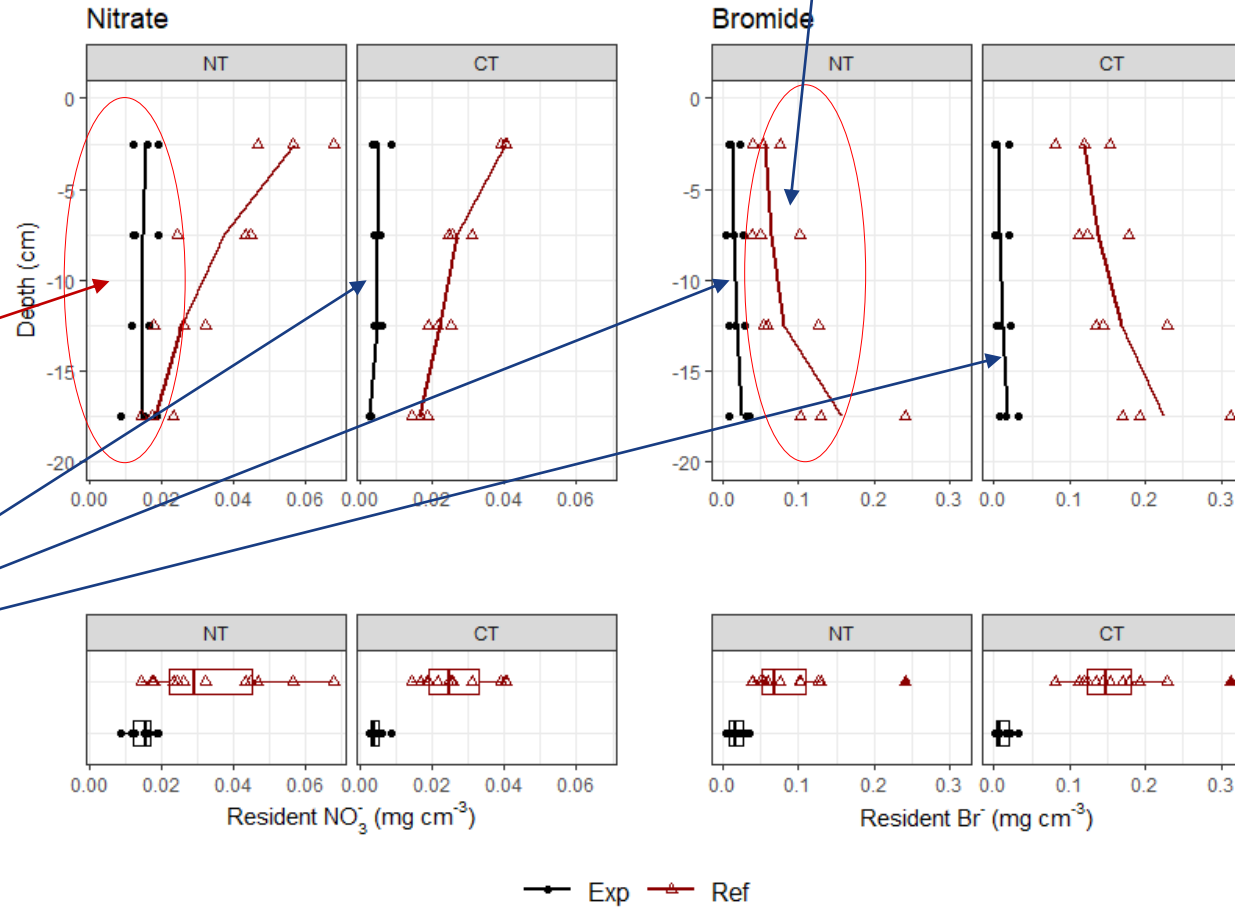
Resident concentrations

- Lower initial Br conc. in NT
- Higher **final** NO_3^- in NT

Bypass of nitrate by macropore flow

No bypass (thorough leaching)

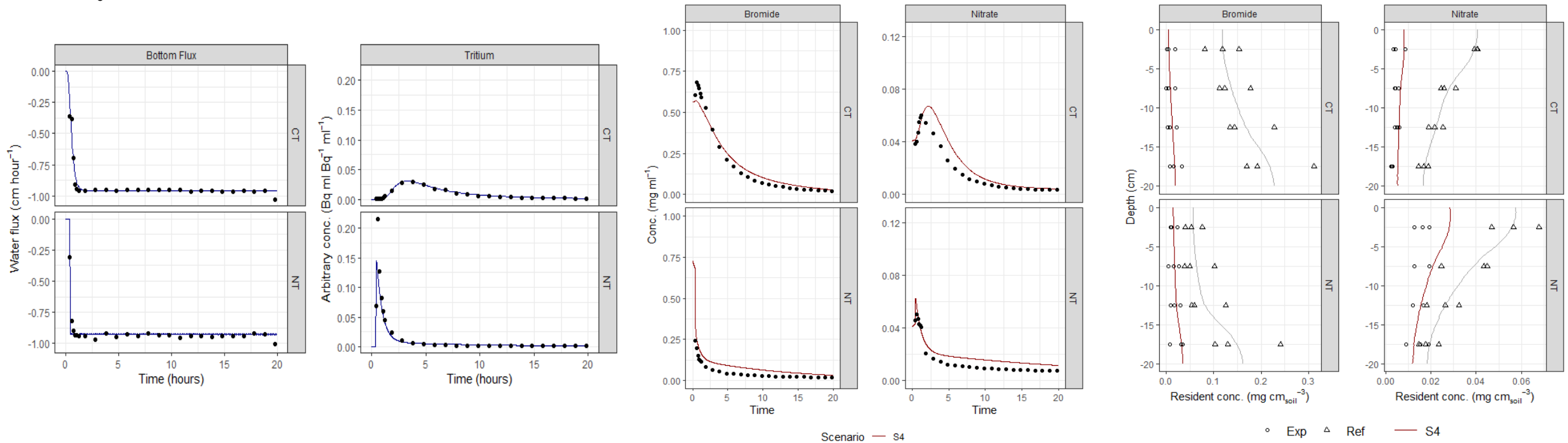
Less Br intrusion in NT



HYDRUS modelling

- $\theta_{\text{sat,mob}} = 0.35$ in CT and $\theta_{\text{sat,mob}} = 0.05$ in NT
- Greater solute transfer coefficients for Br⁻ than NO₃⁻
- Solute distribution close to equilibrium (but not quite)
- The model simulated a bypass effect for NO₃⁻ in NT.

Scenario		Nitrate		Bromide	
		ω_s [T ⁻¹]	RMSE	ω_s [T ⁻¹]	RMSE
CT	S4	0.003	0.0076	0.015	0.0495
NT	S4	0.0075	0.0063	0.025	0.0447



Biopore model in Daisy (1-D)

- Biopores modelled as cylinders
- Sink-source approach
- Biopores activated near saturation
- Critical pressure for deactivation of biopores

Matrix flow and transport

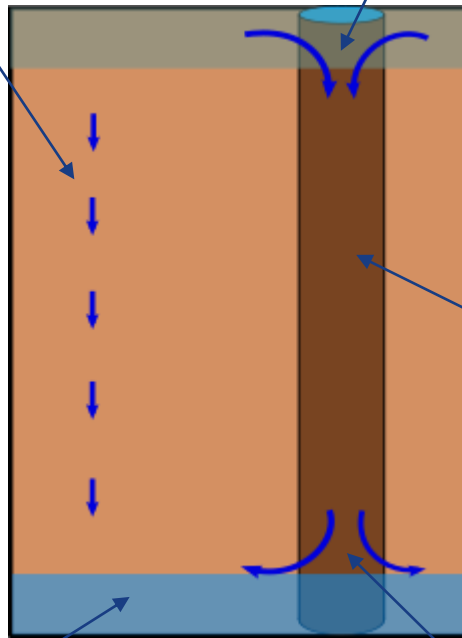
$$\frac{\partial \theta}{\partial t} = \frac{\partial}{\partial z} \left[K(h) \left(\frac{\partial h}{\partial z} + 1 \right) \right] + \Gamma_w$$

$$\frac{\partial \theta c}{\partial t} = \frac{\partial}{\partial z} \left[\theta D \left(\frac{\partial c}{\partial z} \right) \right] - \frac{\partial qc}{\partial z} + \Gamma_s$$

Biopore sink/source

Matrix flow:
Idealized Richard's equation

Biopore sink

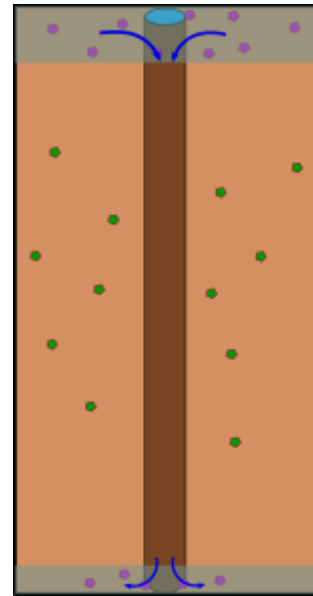


Instantaneous transfer

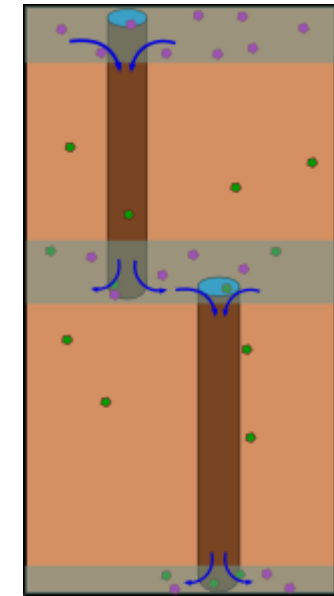
Biopore source

(evt.) saturated matrix

Bypass of matrix by surface solutes and bypass of resident solutes by macropore flow

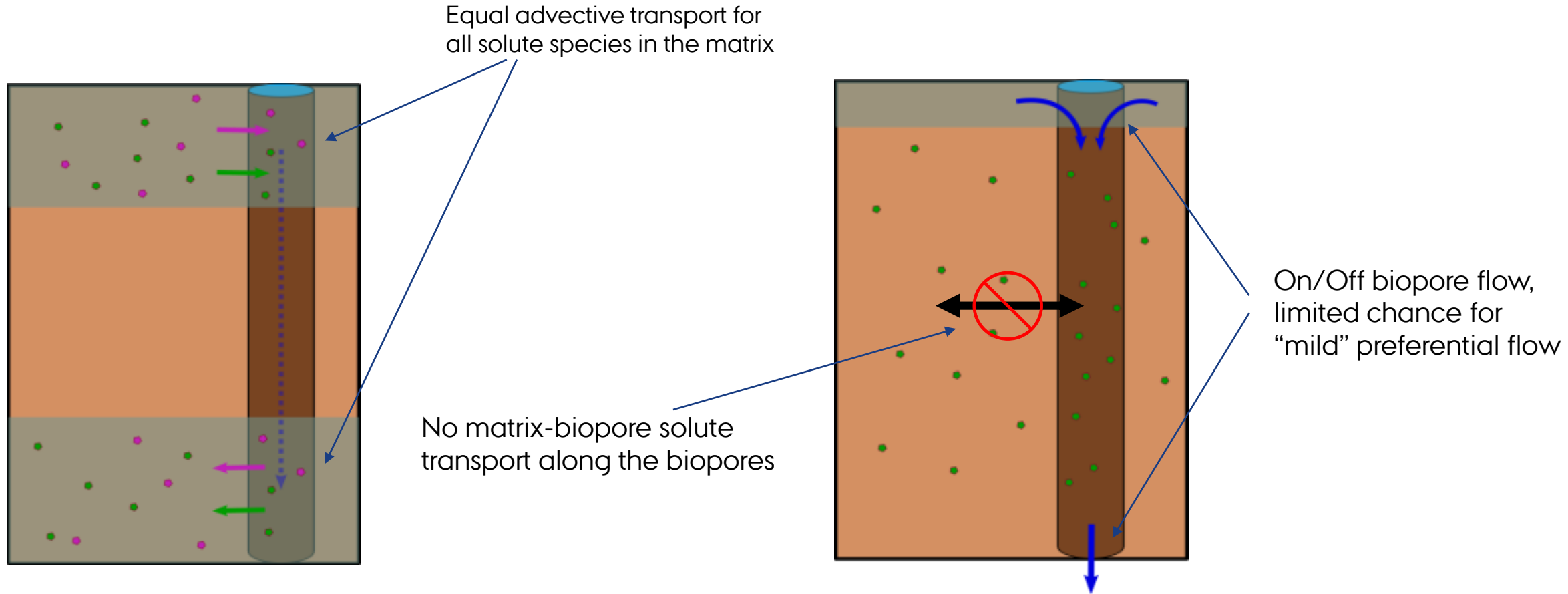


Biopore-matrix interaction at sinks and sources

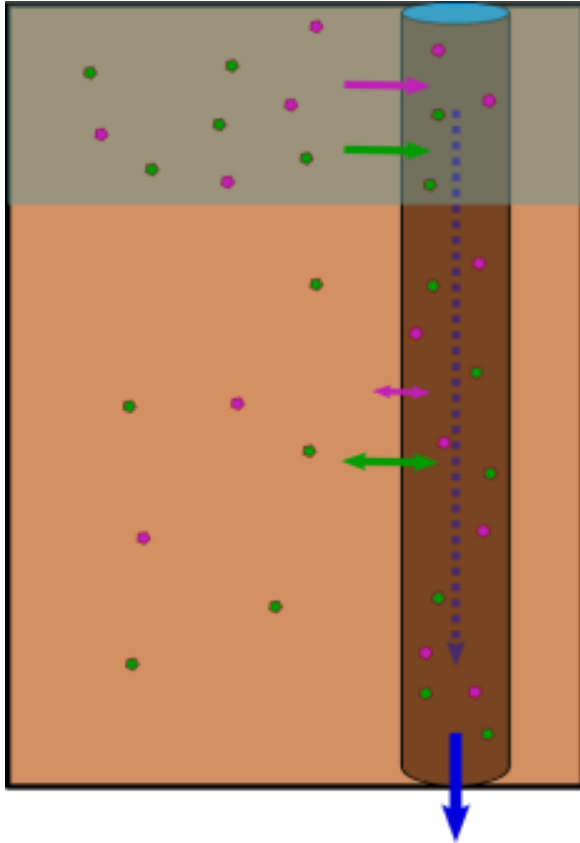


Biopore model in Daisy (1-D) (cont.)

- Water (and) storage



An extended Daisy-like macropore model?



Sink/source and dual-domain hybrid?

- Multiple macropore flow regimes (e.g. different longitudinal dispersivities)
- Matrix-macropore solute transfer along active biopores
- Equilibration of solute concentrations between inactive biopores and matrix



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